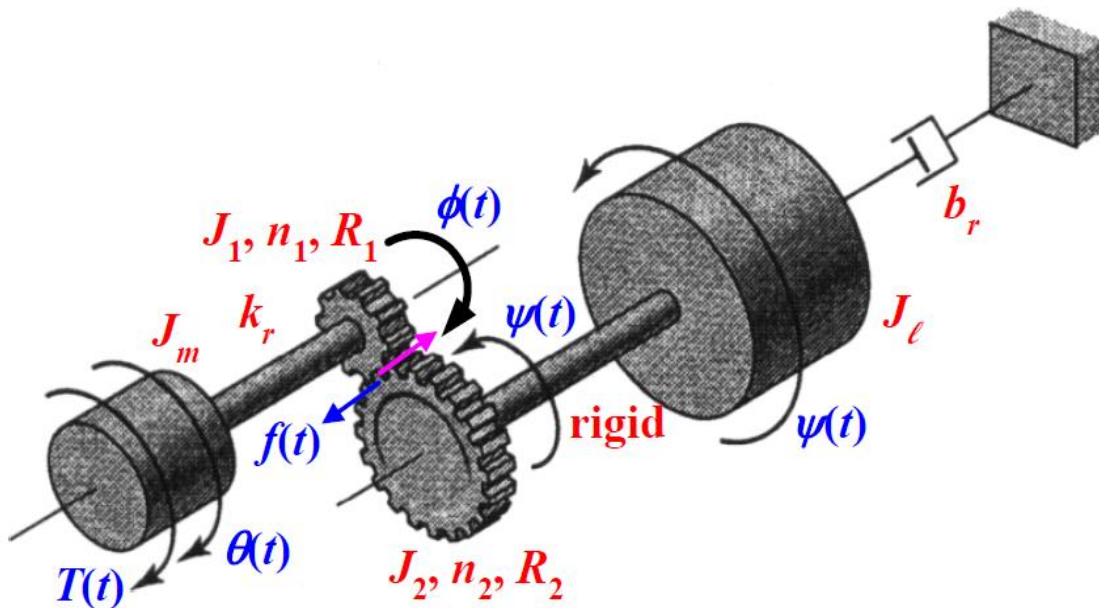


CITY COLLEGE
CITY UNIVERSITY OF NEW YORK
HOMEWORK #4



GEAR- TRAIN MECHANICAL SYSTEM WITH
MOTION INPUT

ME 411: System Modeling Analysis and Control

Fall 2010

Prof. B. Liaw

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October 20, 2010

1.0 Nomenclature

K_R = rotational stiffness

J_m = mass moment of inertia of motor

J_l = mass moment of inertia of load

J_1 = mass moment of inertia of driven spur gear1

J_2 = mass moment of inertia of driven spur gear2

$T(t)$ = intial applied torque caused my motion

$f(t)$ = meshing force between gears

b_r = rotational damping factor

$\theta(t)$ = angular displacement of the motor

$\phi(t)$ = angular displacement of the driven gear 1

$\psi(t)$ = angular displacement of the driven gear 2 and load

R_1 = radius of the gear 1

R_2 = radius of the gear 2

n_1 = number of teeth in gear 1

n_2 = number of teeth in gear 2

n = gear ratio

t = time

$T(s)$ = transferfucntion of the applied torque $T(t)$

$F(s)$ = transferfucntion of the meshing force $f(t)$

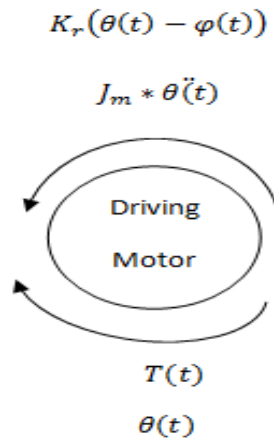
$\Theta(s)$ = transferfucntion of the angular displacement of the motor $\theta(t)$

$\Phi(s)$ = transferfucntion of the angular displacement of the driven gear 1 $\phi(t)$

$\Psi(s)$ = transferfucntion of the angular displacement of the driven gear 2 and load $\psi(t)$

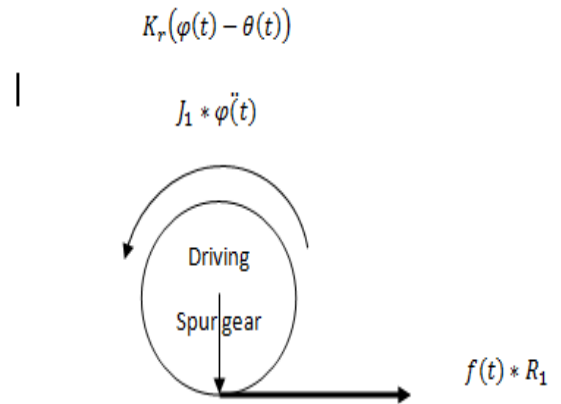
1. FBD

FBD 1.0



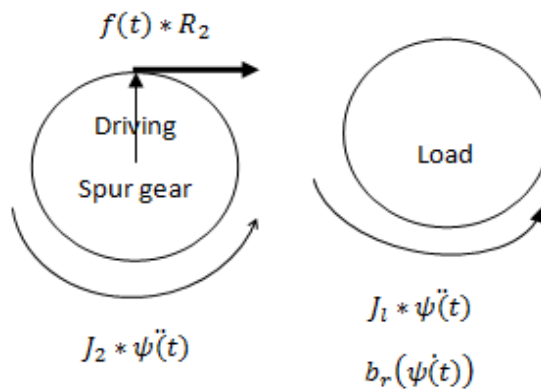
$$J_m * \ddot{\theta}(t) + K_r(\theta(t) - \phi(t)) = T(t)$$

FBD 2.0



$$J_1 * \ddot{\phi}(t) + K_r(\phi(t) - \theta(t)) + f(t) * R_1 = 0$$

FBD 3.0



$$(J_1 + J_2) * \ddot{\psi}(t) + b_r(\dot{\psi}(t)) = f(t) * R_2$$

2. Governing Equations

With the prescribed motion of the motor $\theta(t)$ as the input, set up the necessary free-body diagrams to derive the equations governing the angular displacements, $\phi(t)$ and $\psi(t)$, and the contact force, $f(t)$. Find also the applied torque transfer $T(t)$ required to generate the prescribed motion of the motor $\theta(t)$.

- $J_m * \ddot{\theta}(t) + K_r(\theta(t) - \phi(t)) = T(t)$
- $J_1 * \ddot{\phi}(t) + K_r(\phi(t) - \theta(t)) + f(t) * R_1 = 0$
- $(J_l + J_2) * \ddot{\psi}(t) + b_r(\dot{\psi}(t)) - f(t) * R_2 = 0$

3. Laplace transfer: $\mathcal{L}(\theta(t)) = \Theta(s)$

- $J_m * \ddot{\theta}(t) + K_r(\theta(t) - \phi(t)) = T(t)$

$$T(s) = J_m * s^2 \Theta(s) + K_r \Theta(s) - K_r \Phi(s)$$

- $J_1 * \ddot{\phi}(t) + K_r(\phi(t) - \theta(t)) + f(t) * R_1 = 0$

$$J_1 * s^2 \Phi(s) + K_r \Phi(s) - K_r \Theta(s) + F(s) * R_1 = 0$$

- $(J_l + J_2) * \ddot{\psi}(t) + b_r(\dot{\psi}(t)) - f(t) * R_2 = 0$

$$J_l s^2 \Psi(s) + J_2 s^2 \Psi(s) + b_r s \Psi(s) - F(s) * R_2 = 0$$

Gear ratio:

$$\frac{\phi(t)}{\psi(t)} = \frac{R_2}{R_1} = \frac{n_2}{n_1} = n \text{ and } R_2 = nR_1 \text{ and } \Psi(s) = \frac{\Phi(s)}{n}$$

4. Transfer functions

Solving the equations simultaneous:

$$\Phi(s) = \frac{n^2 * K_r * \Theta(s)}{J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r}$$

$$F(s) = \frac{K_r * \Theta(s) * s * (J_l s + J_2 s + b_r)}{(J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r) * R_1}$$

$$\Psi(s) = \frac{n * K_r * \Theta(s)}{J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r}$$

$$T(s) = J_m * s^2 \Theta(s) + K_r \Theta(s) - \frac{n^2 * K_r^2 * \Theta(s)}{J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r}$$

Transfer function:

$$G_\phi(s) = \frac{\Phi(s)}{\Theta(s)} = \frac{n^2 * K_r}{J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r}$$

$$G_F(s) = \frac{F(s)}{\Theta(s)} = \frac{K_r * s * (J_l s + J_2 s + b_r)}{(J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r) * R_1}$$

$$G_\psi(s) = \frac{\Psi(s)}{\Theta(s)} = \frac{n * K_r}{J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r}$$

$$G_T(s) = \frac{T(s)}{\Theta(s)} = J_m * s^2 + K_r - \frac{n^2 * K_r^2}{J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r}$$

5. Steady state response and analysis:

If the input angular displacement is $\theta(t) = \theta_s \cdot 1(t) = \begin{cases} \theta_s & \text{for } t > 0 \\ 0 & \text{for } t < 0 \end{cases}$, where $1(t)$ is the Heaviside unit step function and θ_s is the step constant, determine the resultant steady-state responses of $\phi(t)$, $\psi(t)$, $f(t)$ and $T(t)$, which are defined as: $\phi_{ss} = \lim_{t \rightarrow \infty} \phi(t)$, $\psi_{ss} = \lim_{t \rightarrow \infty} \psi(t)$, $f_{ss} = \lim_{t \rightarrow \infty} f(t)$, $T_{ss} = \lim_{t \rightarrow \infty} T(t)$ respectively. Provide physical interpretation of your results.

Case 1:

$$\rightarrow \phi_{ss} = \lim_{t \rightarrow \infty} \phi(t) | \theta(t) = \theta_s \cdot 1(t)$$

$$\rightarrow \lim_{s \rightarrow 0} s \frac{\Phi(s)}{\theta(s)} \Big| \cdot \frac{\theta_s}{s}$$

$$\rightarrow \lim_{s \rightarrow 0} s \frac{n^2 * K_r}{J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r} \frac{\theta_s}{s} \rightarrow \theta_s$$

This implies physically that as the time tends to infinity and the body reaches a steady state the output angular motion of the gear1 will be same as that of the input value.

Case 2:

$$\rightarrow \psi_{ss} = \lim_{t \rightarrow \infty} \psi(t) | \theta(t) = \theta_s \cdot 1(t)$$

$$\rightarrow \lim_{s \rightarrow 0} s \frac{\Psi(s)}{\theta(s)} \Big| \cdot \frac{\theta_s}{s}$$

$$\rightarrow \lim_{s \rightarrow 0} s \frac{n * K_r}{J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r} \frac{\theta_s}{s} \rightarrow \frac{\theta_s}{n}$$

This implies physically that as the time tends to infinity and the body reaches a steady state the output angular motion of the gear2 will be the ratio of the input value over the gear ration. This means the gear teeth, radius play a very important role in power transmission.

Case 3:

$$\rightarrow f_{ss} = \lim_{t \rightarrow \infty} f(t) | \theta(t) = \theta_s \cdot 1(t)$$

$$\rightarrow \lim_{s \rightarrow 0} s \frac{F(s)}{\Theta(s)} \Big| \cdot \frac{\theta_s}{s}$$

$$\rightarrow \lim_{s \rightarrow 0} s \frac{K_r * (J_1 s + J_2 s + b_r) * s}{(J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r) * R_1} \frac{\theta_s}{s} = \mathbf{0}$$

This implies physically that as the time tends to infinity and the body reaches a steady state, the meshing force between the teeth of the gear becomes zero an ideal stage.

Case 4:

$$\rightarrow T_{ss} = \lim_{t \rightarrow \infty} T(t) | \theta(t) = \theta_s \cdot 1(t)$$

$$\rightarrow \lim_{s \rightarrow 0} s \frac{T(s)}{\theta(s)} \Big| \cdot \frac{\theta_s}{s}$$

$$\rightarrow \lim_{s \rightarrow 0} s \left(J_m * s^2 + K_r - \frac{n^2 * K_r^2}{J_l * s^2 + J_2 * s^2 + b_r * s + n^2 * J_1 * s^2 + n^2 * K_r} \right) \frac{\theta_s}{s} \rightarrow \mathbf{\theta_s * (K_r - 1)}$$

6. MATLAB solutions for the zeros and poles (i.e., the characteristic roots) for four transform functions. Assume the following data:

J_m	J_l	J_1	J_2	R_1	R_2	K_r	b_r
[kg-m ²]	[kg-m ²]	[kg-m ²]	[kg-m ²]	m	m	[N-m]	[N-m]/s
0.04	0.08	0.01	0.02	0.1	0.2	0.3	0.2

Definition 1: *zeros*

1. The value(s) for z where the *numerator* of the transfer function equals zero
2. The complex frequencies that make the overall gain of the filter transfer function zero.

Definition 2: *poles*

1. The value(s) for z where the *denominator* of the transfer function equals zero
2. The complex frequencies that make the overall gain of the filter transfer function infinite.

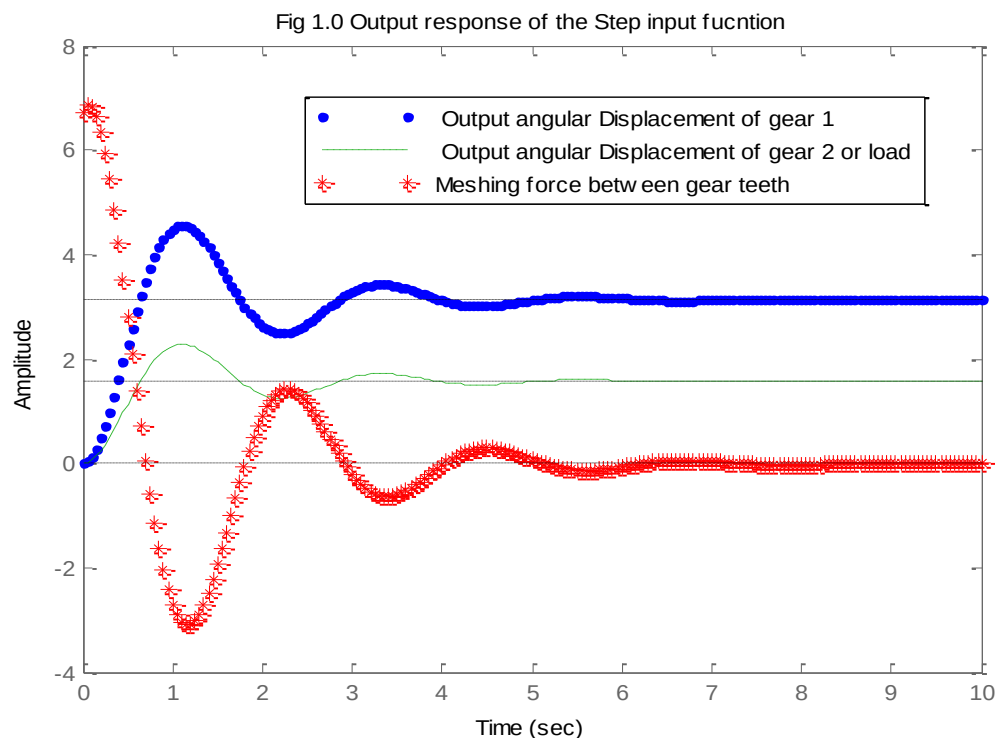
<i>Transfer Function</i>	<i>Zeros (z)</i>	<i>Poles (p)</i>
$G_\phi(s) = \frac{1.20}{0.140 * s^2 + 0.2 * s + 1.20}$		- 0.7143 + 2.8392i - 0.7143 - 2.8392i
$G_F(s) = \frac{0.3 * s^2 + 0.6 * s}{0.140 * s^2 + 0.2 * s + 1.20}$	0 -2	- 0.7143 + 2.8392i - 0.7143 - 2.8392i
$G_\Psi(s) = \frac{0.6}{0.140 * s^2 + 0.2 * s + 1.20}$		- 0.7143 + 2.8392i - 0.7143 - 2.8392i
$G_T(s) = \frac{0.0056 * s^4 + 0.008 * s^3 + 0.09 * s^2 + 0.06 * s}{0.140 * s^2 + 0.2 * s + 1.20}$	0 -0.37 + 3.9275i -0.37 - 3.9275i -0.6885	- 0.7143 + 2.8392i - 0.7143 - 2.8392i

7. MATLAB solutions for transient responses. Use MATLAB to find the responses $\phi(t)$, $\psi(t)$ and $f(t)$ due to various prescribed motions $\theta(t)$ listed below. For each case, plot the time histories of $\phi(t)$, $\psi(t)$, $f(t)$ and $\theta(t)$ on the same graph. For the first three sub cases, determine also the corresponding poles and residues using the MATLAB command: **residue**. Data of additional parameters needed for calculations are tabulated below.

θ_s	θ_r	θ_d	θ_p	t_p	θ_{tr}	t_{tr}
[rad]	[rad/s]	[deg-s]	[rad]	[s]	[rad]	[s]
π	0.1π	π	π	5	π	5

7.1 Step input: $\theta(t) = \theta_s \cdot 1(t) = \begin{cases} \theta_s & \text{for } t > 0 \\ 0 & \text{for } t < 0 \end{cases}$, where θ_s is the step constant.

Compute and plot the results for a duration of 10 s. Determine also the poles and residues of $\Phi(s)$, $\psi(s)$ and $F(s)$, respectively, corresponding to this input motion. Use the MATLAB command: **Itiview** to determine the peak amplitudes, maximum overshoots in %, peak times, 0-100% rise times, $\pm 2\%$ settling times and steady-state values of the responses $\phi(t)$, $\psi(t)$ and $f(t)$, respectively. Compare the graphical results with those of Part (d).



$$\Phi(s) = \frac{188.4955592}{7 * s^2 + 10 * s + 60}$$

RESIDUE: 0 - 4.7414i

0 + 4.7414i

POLES: -0.7143 + 2.8392i

-0.7143 - 2.8392i

$$\Psi(s) = \frac{94.24777962}{7 * s^2 + 10 * s + 60}$$

RESIDUE: 0 - 2.3709i

0 + 2.3709i

POLES: -0.7143 + 2.8392i

-0.7143 - 2.8392i

$$F(s) = \frac{47.12388981s^2 + 94.24777962s}{7 * s^2 + 10 * s + 60}$$

RESIDUE: 1.9233 +10.6447i

1.9233 -10.6447i

POLES: -0.7143 + 2.8392i

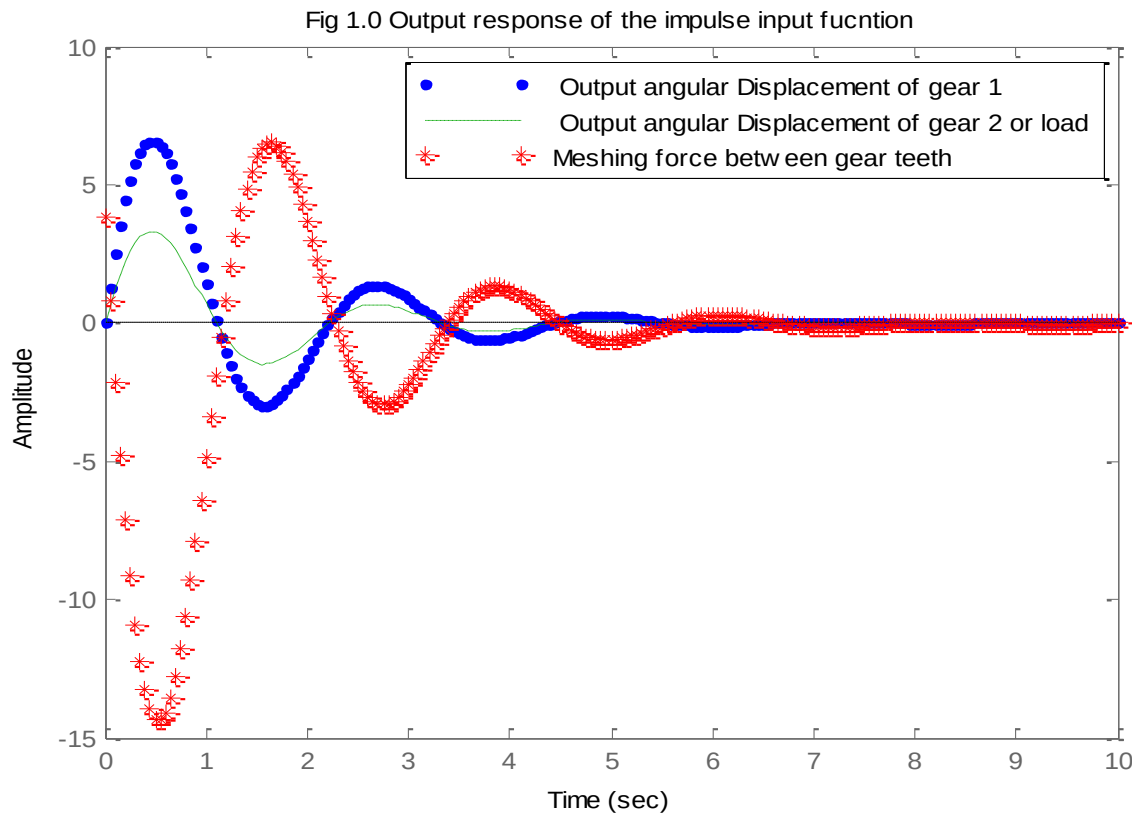
-0.7143 - 2.8392i

Output	Peak Amplitudes	Maximum Overshoots in %	Peak Times	0-100% Rise Times	±2% Settling Times	Steady State	Steady State (d)
$\phi(t)$	4.57	45.4	1.1	0.6408	4.8335	3.14	π
$\psi(t)$	2.28	45.4	1.1	0.6408	4.8335	1.57	$\pi/2$
$f(t)$	6.85	infinity	0.05	0.7039	4.8965	0	0

7.2 Impulse input: $\theta(t) = \theta_\delta \cdot \delta(t) = \begin{cases} \infty & \text{for } t = 0 \\ 0 & \text{for } t \neq 0 \end{cases}$, where $\delta(t)$ is the unit impulse

function (also called Dirac Delta function) and constant θ_δ is the impulse strength.

Compute and plot the results for a duration of 10 s. Determine also the poles and residues of $\Phi(s)$, $\psi(s)$ and $F(s)$, respectively, corresponding to this input motion. Use the MATLAB command: **ltiview** to determine the peak amplitudes, peak times and $\pm 2\%$ settling times of the responses $\varphi(t)$, $\psi(t)$ and $f(t)$, respectively.



$$\Phi(s) = \frac{188.4955592}{7 * s^2 + 10 * s + 60}$$

RESIDUE: 0 - 4.7414i

0 + 4.7414i

POLES: -0.7143 + 2.8392i

-0.7143 - 2.8392i

$$\Psi(s) = \frac{94.24777962}{7 * s^2 + 10 * s + 60}$$

RESIDUE: 0 - 2.3709i
0 + 2.3709i

POLES: -0.7143 + 2.8392i
-0.7143 - 2.8392i

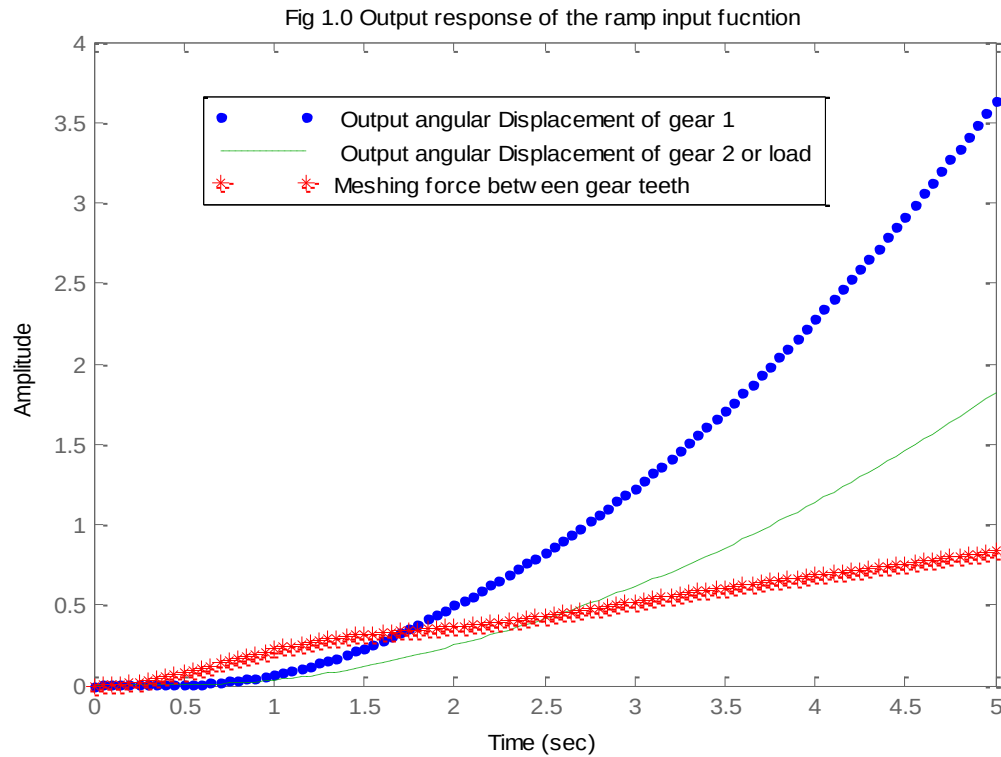
$$F(s) = \frac{47.12388981s^2 + 94.24777962s}{7 * s^2 + 10 * s + 60}$$

RESIDUE: 1.9233 +10.6447i
1.9233 -10.6447i

POLES: -0.7143 + 2.8392i
-0.7143 - 2.8392i

<i>Output</i>	<i>Peak Amplitudes</i>	<i>Peak Times</i>	<i>±2% Settling Times</i>	<i>Steady State</i>	<i>Steady State (d)</i>
$\phi(t)$	6.58	0.45	5.3	0	π
$\psi(t)$	3.29	0.45	5.3	0	$\pi/2$
$f(t)$	-14.3	0.55	5.36	0	0

7.3 Ramp input: $\theta(t) = \theta_r t. 1(t) = \begin{cases} \theta_r t & \text{for } t > 0 \\ 0 & \text{for } t < 0 \end{cases}$, where the constant θ_r is the ramp slope. Compute and plot the results for a duration of 5 s. Determine also the poles and residues of $\Phi(s)$, $\psi(s)$ and $F(s)$, respectively, corresponding to this input motion.



$$\Phi(s) = \frac{18.84955592}{s^3 * (7.* s^2 + 10.* s + 60.)}$$

RESIDUE: 0.0262 + 0.0487i
0.0262 - 0.0487i
-0.0523
0.3140

POLES: -0.7143 + 2.8392i
-0.7143 - 2.8392i
0
0

$$\Psi(s) = \frac{9.424777962}{s^3 * (7.* s^2 + 10.* s + 60.)}$$

RESIDUE: 0.0131 + 0.0244i
0.0131 - 0.0244i
-0.0262
0.1571

POLES: -0.7143 + 2.8392i
-0.7143 - 2.8392i
0
0

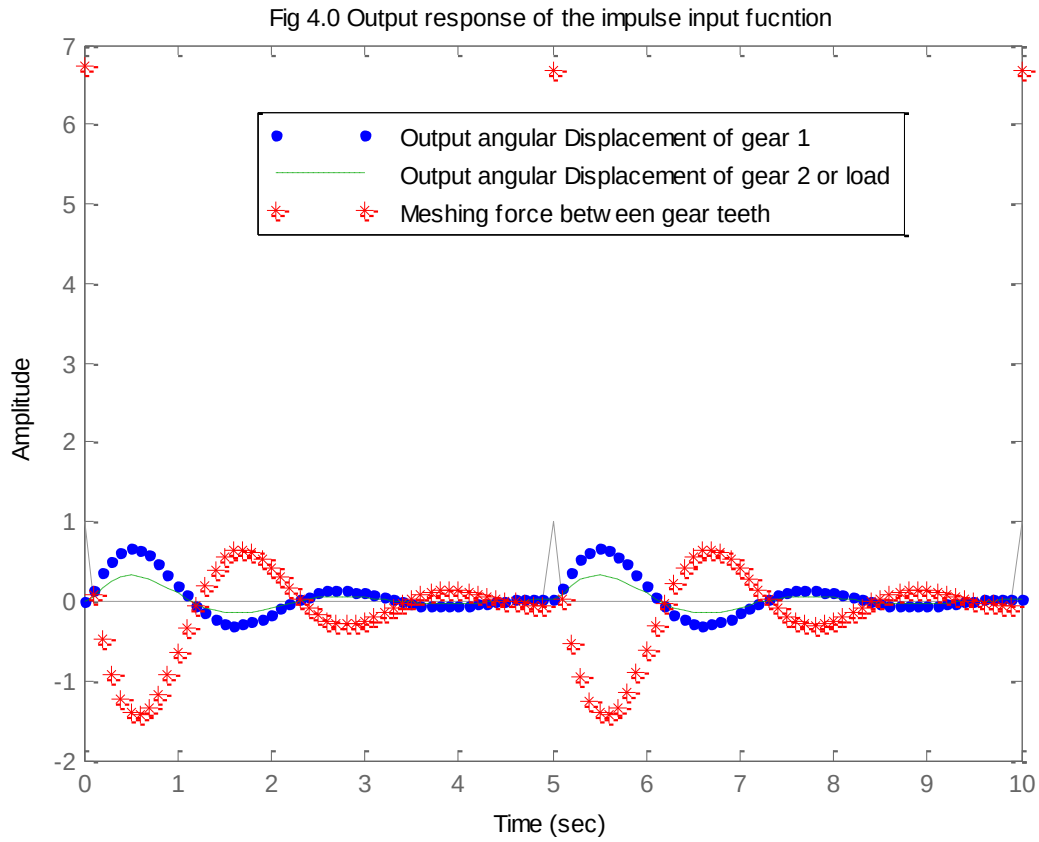
$$F(s) = \frac{4.712388981 * (s + 2.)}{s * (7.* s^2 + 10.* s + 60.)}$$

RESIDUE: -0.0785 - 0.0988i
-0.0785 + 0.0988i
0.1571

POLES: -0.7143 + 2.8392i
-0.7143 - 2.8392i
0

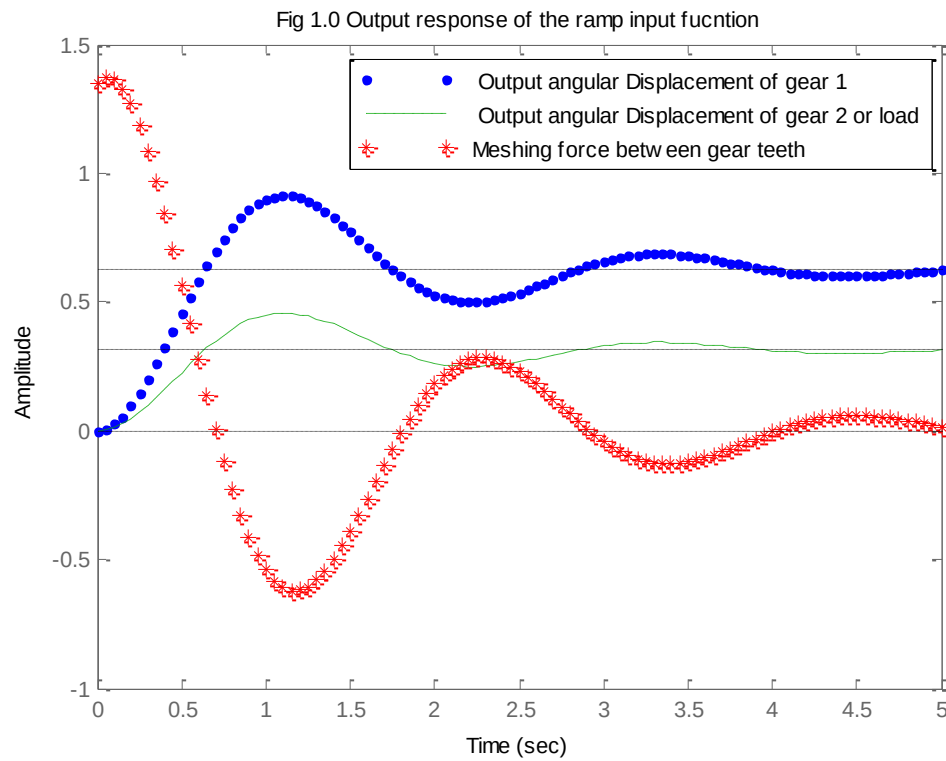
7.4 Pulse input: $\theta(t) = \begin{cases} 0 & t_p < t \\ \theta_p & \text{when } 0 < t < t_p \\ 0 & t < 0 \end{cases}$, where the two constant θ_p and t_p are

the pulse strength and pulse duration, respectively. Compute and plot the results for duration of 10s.



7.5 Terminated –ramp input: $\theta(t) = \begin{cases} \theta_{tr} & t_{tr} < t \\ \frac{\theta_{tr}}{t_{tr}}t & \text{when } 0 < t < t_{tr} \\ 0 & t < 0 \end{cases}$, ,where the two

constant θ_{tr} and t_{tr} are the terminated step and ramp duration, respectively. Compute and plot the results for duration of 5s.



8. MATLAB solutions for applied torque. Use MATLAB to find the applied torque $T(t)$ needed to generate the prescribed motions given in Part (e). If you encounter difficulty, state the reason why.

$$T(s) = \frac{.87964 * s^4 + 1.2566 * s^3 + 14.137 * s^2 + 9.424 * s}{7s^2 + 10s + 60}$$

$$T(t) = \frac{1616331 * \text{dirac}(t)}{1715000} - \frac{\text{dirac}(t, 1)}{245000} + \frac{21991 * \text{dirac}(t, 2)}{175000} - \frac{73 * \left(\cos\left(\frac{395\frac{1}{2} * t}{7}\right) + \frac{67885537 * 395\frac{1}{2} * \sin\left(\frac{395\frac{1}{2} * t}{7}\right)}{28835} \right)}{1200500 * \exp\left(\frac{5 * t}{7}\right)}$$

Unable to evaluate the function, Numerical Solutions out of range.

9. Appendix

MATLAB Code for Unit Step input

```
clear all
clc
t=0:0.05:10;

Phi_num=188.495592;
Phi_den=[7 10 60];
transfer_Phi = tf(Phi_num, Phi_den);

Psi_num=94.24777962;
Psi_den=[7 10 60];
transfer_Psi = tf(Psi_num, Psi_den);

force_num=[47.12388981 94.2477962 0];
force_den=[7 10 60];
transfer_Force = tf(force_num, force_den);

step(transfer_Phi, 'b.', transfer_Psi, 'g--', transfer_Force, 'r*', t)
title('Fig 1.0 Output response of the Step input fuction')
legend('    Output angular Displacement of gear 1', '    Output angular Displacement of gear 2 or load', '    Meshing force between gear teeth')

%Rise time (0-100%)
%settling time (+-2%)
    %SettlingTime – Settling time
    %SettlingMin – Minimum value of y once the response has risen
    %SettlingMax – Maximum value of y once the response has risen
    %Overshoot – Percentage overshoot (relative to yfinal)
    %Undershoot – Percentage undershoot
    %Peak – Peak absolute value of y
    %PeakTime – Time at which this peak is reached

S_Phi = stepinfo(transfer_Phi, 'RiseTimeLimits', [0,1])
S_Psi = stepinfo(transfer_Psi, 'RiseTimeLimits', [0,1])
S_Force = stepinfo(transfer_Force, 'RiseTimeLimits', [0,1])
```

MATLAB Code for Impulse input

```
clear all
clc
t=0:0.05:10;

Phi_num=188.495592;
Phi_den=[7 10 60];
transfer_Phi = tf(Phi_num, Phi_den);

Psi_num=94.24777962;
Psi_den=[7 10 60];
transfer_Psi = tf(Psi_num, Psi_den);
```

```

force_num=[47.12388981 94.2477962 0];
force_den=[7 10 60];
transfer_Force = tf(force_num, force_den);

impulse(transfer_Phi, 'b.', transfer_Psi, 'g--', transfer_Force, 'r*', t)
title('Fig 1.0 Output response of the impulse input fucntion')
legend('    Output angular Displacement of gear 1', '    Output angular
Displacement of gear 2 or load', '    Meshing force between gear teeth')

```

MATLAB Code for Ramp input

```

clear all
clc
t=0:0.05:5;

Phi_num=18.8495592;
Phi_den=[7 10 60 0 0];
transfer_Phi = tf(Phi_num, [Phi_den 0]);

Psi_num=9.424777962;
Psi_den=[7 10 60 0 0];
transfer_Psi = tf(Psi_num, [Psi_den 0]);

force_num=[4.712388981 9.42477962];
force_den=[7 10 60 0];
transfer_Force = tf(force_num, [force_den 0]);

impulse(transfer_Phi, 'b.', transfer_Psi, 'g--', transfer_Force, 'r*', t)
title('Fig 1.0 Output response of the ramp input fucntion')
legend('    Output angular Displacement of gear 1', '    Output angular
Displacement of gear 2 or load', '    Meshing force between gear teeth')

```

MATLAB Code for Pulse input

```

clear all
clc
[theta,t] = gensig('Pulse',5,10,0.1);

Phi_num=188.495592;
Phi_den=[7 10 60];
transfer_Phi = tf(Phi_num, Phi_den);

Psi_num=94.24777962;
Psi_den=[7 10 60];
transfer_Psi = tf(Psi_num, Psi_den);

force_num=[47.12388981 94.2477962 0];
force_den=[7 10 60];
transfer_Force = tf(force_num, force_den);
lsim(transfer_Phi, 'b.', transfer_Psi, 'g--', transfer_Force, 'r*', theta, t)
title('Fig 4.0 Output response of the impulse input fucntion')
legend('    Output angular Displacement of gear 1', '    Output angular
Displacement of gear 2 or load', '    Meshing force between gear teeth')

```